

# The Critical Assessment of the Experimental Techniques for Cardiac Performance

Pages with reference to book, From 18 To 25

Shahid Rashid ( Department of Pharmacology, University of Karachi, Karachi. )

Naeema Ansari ( Department of Physiology, Sind Medical College, Karachi. )

## Abstract

Classical haemodynamics has been notably successful in defining the normal physiology of the Cardiovascular system, but failed to provide a clear definition and early diagnosis of a functional impairment of the myocardium, this failure is possibly attributable to inadequacy of the monitored variables of the conventional haemodynamics studies.

In this article, two common parameters of cardiodynamics, viz., cardiac output and first derivatives of the ventricular pressure ( $dP/dt$ ), are discussed in order to find properties of cardiac muscle which could help in distinguishing alterations of ventricular performance (JPMA: 33:18, 1983).

## Introduction

Classical haemodynamics, notably successful in defining the normal physiology of the cardiovascular system as well as the pathophysiology of congenital heart disease, has yet failed to provide a clear definition and early diagnosis of a functional impairment of the myocardium. This failure could be due to inadequacy of the monitored variables of the conventional haemodynamics studies. Apart from the parameters of haemodynamics such as blood pressure and mean blood flow, which are very indirect and insensitive indicators of myocardial function, parameters such as mean systolic ejection rate, stroke work and power and  $dP/dt$  are equally wanting.

These considerations combined with the development of new techniques aroused the interest of physiologists to appreciate that the heart is not only a pump but is also a muscle, the evaluation of whose properties could help in distinguishing alterations of ventricular performance. The following list of parameters of cardiac function shows some commonly used but not very sensitive expressions and also includes the recent and specific indices in which both pressure and volume have been used.

1. Cardiac output (C.O.) and stroke volume.
2. Mean systolic ejection rate.
3. Left ventricular work and contractility index.
4. Ventricular power.
5. Systolic time intervals.
6. Indices of cardiac response to exercise.
7. Ventricular volume and ejection fraction.
8. Left ventricular mass.
9. First derivatives of the ventricular pressure ( $dP/dt$ ).
10. Haemodynamic correlates of myocardial  $O_2$  consumption.
11. External mechanical efficiency.

All these parameters are significant in the assessment of cardiac performance, but C.O. and first derivatives of the ventricular pressure will be discussed here in detail.

I. Cardiac Output (C.O.):— CO. is defined as the amount of blood ejected per unit of time ( $m^3/min$ ).

Commonly used as an index of ventricular function, the C.O. is a relatively insensitive parameter for its assessment, being regulated by various factors, such as body  $O_2$  requirement, venous return,

mechanical loads and myocardial mass (Kelman, 1971). The C.O. of a normal man at rest is approximately 5 Lit/min but under different physiological conditions this value changes, e.g., during certain forms of anaesthesia C.O. may fall to 2.5 L/min (Kelman, 1971), whereas it may increase to as high as 30 L/min during strenuous exercise (Astrand et al., 1964).

Several methods are available for the indirect measurement of C.O. but the FICK and indicator dilution methods are the standard techniques for the measurement of C.O. because of their accuracy, safety, reproducibility and simplicity (Yang et al., 1972a). These two, along with other methods will be

discussed in detail.

1. Direct Fick Method. (Fick, 1870):- Blood flow through an organ can be determined if a substance is removed from or added to the blood during its flow through the organ. The above Fick principle has been used in lungs to calculate the volume of the blood required transport the  $O_2$  taken up from the alveoli per unit time. The direct Fick method employs the following formula  $C.O. = \frac{O_2 \text{ Consumption}}{A - V_2} \times 100$

**A-V<sub>2</sub> difference**

$O_2$  consumption is generally measured over a period of several minutes. A preferred technique is to collect all the expired air in spirometer over a timed period (usually 3 min and analysing samples for  $O_2$  content in expired air. Comparison between  $O_2$  contents in expired air and ambient air (volume should be the same in both cases) provides the data required to compute the  $O_2$  uptake.  $O_2$

consumption can also be measured with Nunn's technique, the subject inspires an appropriate gas mixture from a rigid airtight box and then expires into a bag contained within the box. The change of volume of the total bag-box gives a measure of the difference between inspired and expired minute volume (Kelman, 1971).

$$C.O. = \frac{I \times 60}{A/B \times K \times t} = \frac{C \times 60}{Area \times t}$$

C.O. = Cardiac output

I = Amount of the indicator injected (mg)

60 = 60 sec/min.

A = Area under the complete curve (mm<sup>2</sup>)

B = Base of the complete curve (mm)

K = Calibration factor mg/l/mm

t = Total curve duration (Sec)

Arteriovenous oxygen difference (A-VO<sub>2</sub>) :-The arterial blood throughout the body normally has a uniform  $O_2$  content. However to determine a significant A-VO<sub>2</sub> difference it is necessary to know the content of  $O_2$  in mixed venous blood. The mixed venous blood is preferably sampled from the pulmonary artery where the mixing is adequate, to gain the samples, a catheter is based through the venous channels into the right chambers of the heart.

$$\begin{aligned}
 \text{C.O.} &= \frac{I \times 60}{\text{cm} \times t} = \frac{I \times 60}{\text{Area}} = \frac{I \times 60}{\text{PC} \times \text{PCT}} \\
 &= \frac{(C \times 60)}{\text{PC} \times \text{PCT}} \quad \frac{3-0.9 (\text{PCT}/\text{AT})}{3-0.9 (\text{PCT}/\text{AT})} \\
 \text{Flow } F &= \frac{m \times 60 (T_2 - T_1) \times \text{SHR} \times \text{SGR}}{A \times f}
 \end{aligned}$$

- where
- $m$  = mass of injectate
  - $T_1$  = Temperature of saline
  - $T_2$  = Temperature of the body of the animal
  - $\text{SHR}$  = Ratio of the specific heats of the blood and injectate
  - $\text{SGR}$  = Ratio of the specific gravity of the blood and injectate
  - $A$  = Area under the thermodilution curve
  - $f$  = Constant

The cardiac catheterization is not free from dangers in that it can produce ventricular fibrillation (Bousvaros et al., 1962). The technique of cardiac catheterization and its source of error have been described in detail by Stow (1954). However, the catheterization of the right heart in order to obtain samples of mixed venous blood is a disadvantage (Kelman, 1971).

Arterial and venous  $O_2$  content can be directly measured with van Slyke apparatus. This method though is very accurate, carried out by a highly trained person, but is time consuming. For rapid determination of blood  $O_2$  contents, photo-electric method compares favourably with van Slyke method.

Apart from the cardiac catheterization as a disadvantage, there are few more considerations to test the validity of this method. Cardiac catheterization itself is too complicated a procedure to use in routine studies and is not entirely suitable for use during exercise. The other assumption in this technique that the rate of  $CO_2$  removal by the blood equals the rate of  $CO_2$  uptake at the mouth does not apply at the start of exercise. The composition of arterial blood varies during respiratory or cardiac cycle. These variations may cause errors in the calculated  $CO$  in rest as well as in exercise.

**2. Indicator Dilution Method :-** In recent years the Fick technique has been challenged by the introduction of the indicator dilution method, being easier to use and not requiring either samples of mixed venous blood or the measurement of the body  $O_2$  consumption which may be experimentally difficult particularly during anaesthesia.

Introduced by Stewart (1897) this method was based on the principle that volume of a fluid in a container can be calculated by adding a known quantity of dye and measuring the concentration of the material following even dispersal through the fluid. The volume can be calculated by the formula:-

$$V = \frac{A}{C}$$

where  $V$  = volume of the fluid

$A$  = amount of dye added

And  $C$  = concentration of the dye in each cubic centimeter of fluid.

Stewart (1921), showed that his method can also be applied to fluids in motion. Its usefulness was confirmed by Kinman et al. (1929) and Hamilton and Remington (1948), and its theoretical validity shown by Zierler

(1962). This method employs the Hamilton equation which is as follows:-

$PC$  = Peak Concentration.

$PCT$  = Peak Concentration Time.

The dotted line is the terminal portion of the indicator dilution curve expected to be without recirculation.

A bolus injection of a certain amount of dye is given into the circulation via the jugular vein of the right side of the heart and blood is withdrawn through brachial artery at a constant rate. A time concentration curve can be recorded using a densitometer (Fig. 1).

$$C.O. = \frac{I \times 60}{C_m \times t}$$

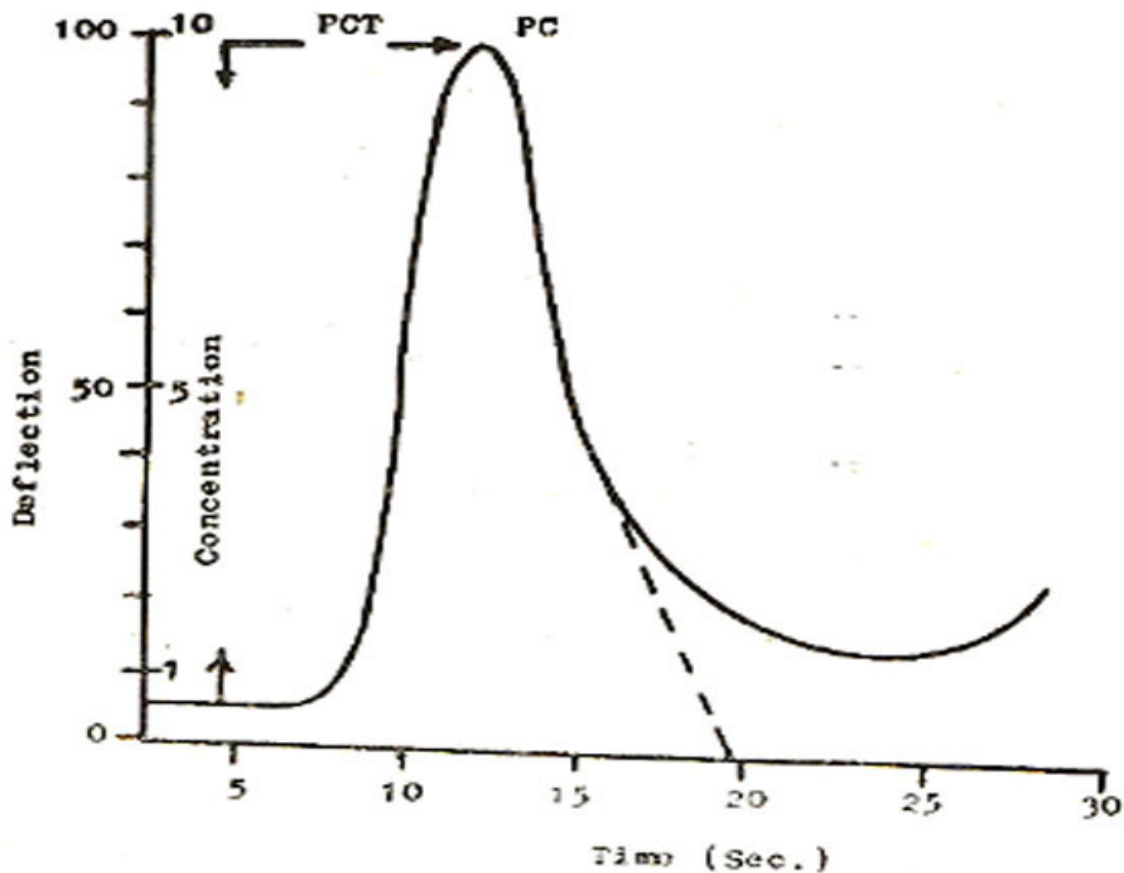
CO = Cardiac output (l/min)

I = Amount of indicator injected (mg)  
60 — 60 sec/min

C<sub>m</sub> = Mean indicator concentration

t = Total curve duration.

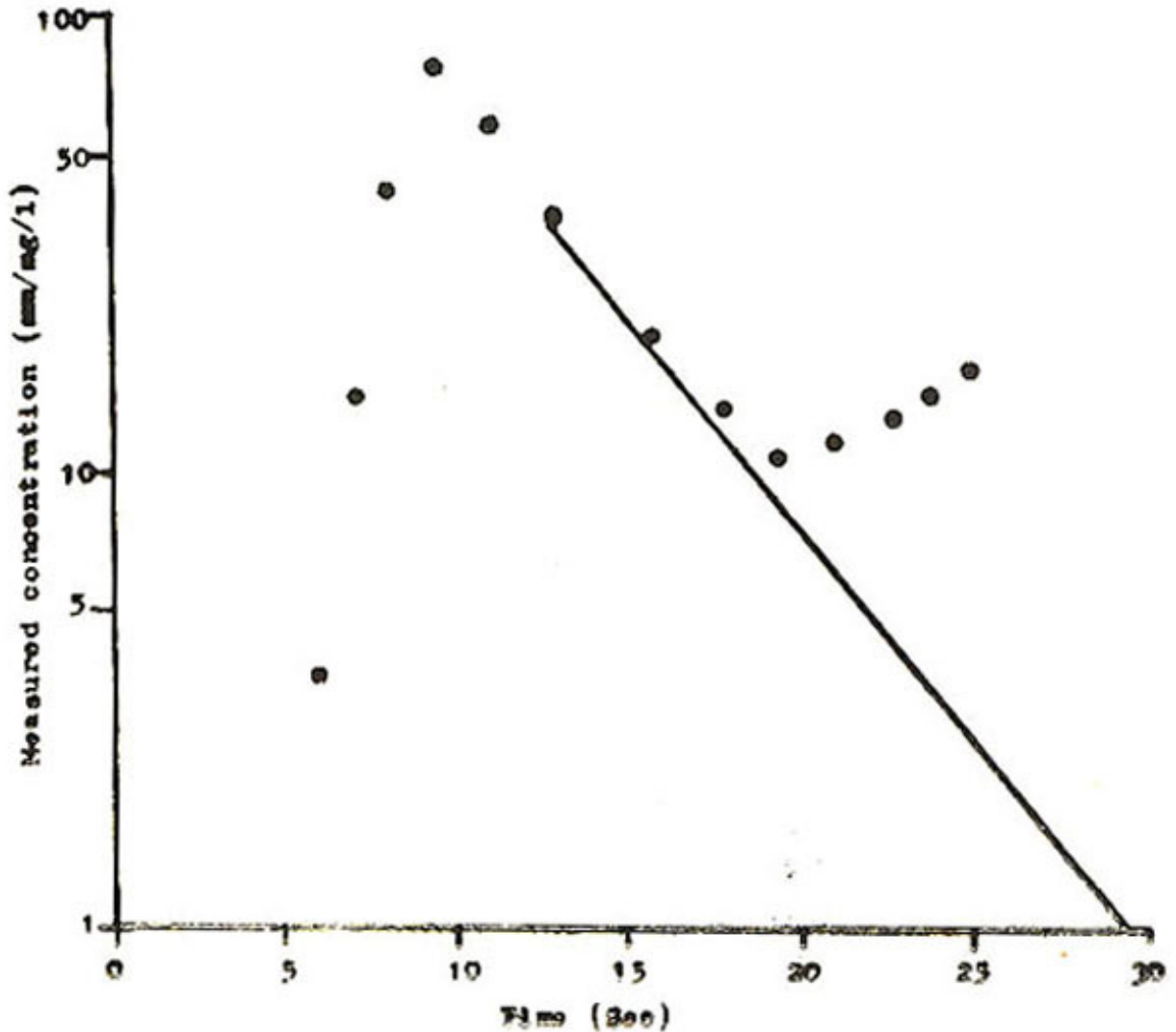
mg/l



*Fig. 1.* Shows the Indicator (dye) Concentration (mg/L) measured as a Deflection on the Original Curve (in m.m.).

The rapid injection of indicator causes a sudden, transient high concentration of the dye in the venous blood. By the time the indicator has reached the arterial side of the circulation this concentration profile has become flattened and prolonged because different particles of blood take different pathways through the pulmonary circulation.

The time-concentration curve consists of initial rapidly ascending phase followed by a slower downstroke and a secondary recirculation curve, which occurs before the first pass effect has had time to fully decay. This recirculation curve poses a difficulty in the assessment of the mean indicator concentration. This difficulty can be overcome by extrapolating the descending limb towards the base. For practical purposes a point at which the indicator concentration is 1% of the peak concentration is (arbitrarily) chosen as the end of the disappearance time. The indicator dilution curve replotted on semilogarithmic paper is, therefore, extrapolated to this point (Fig. 2).



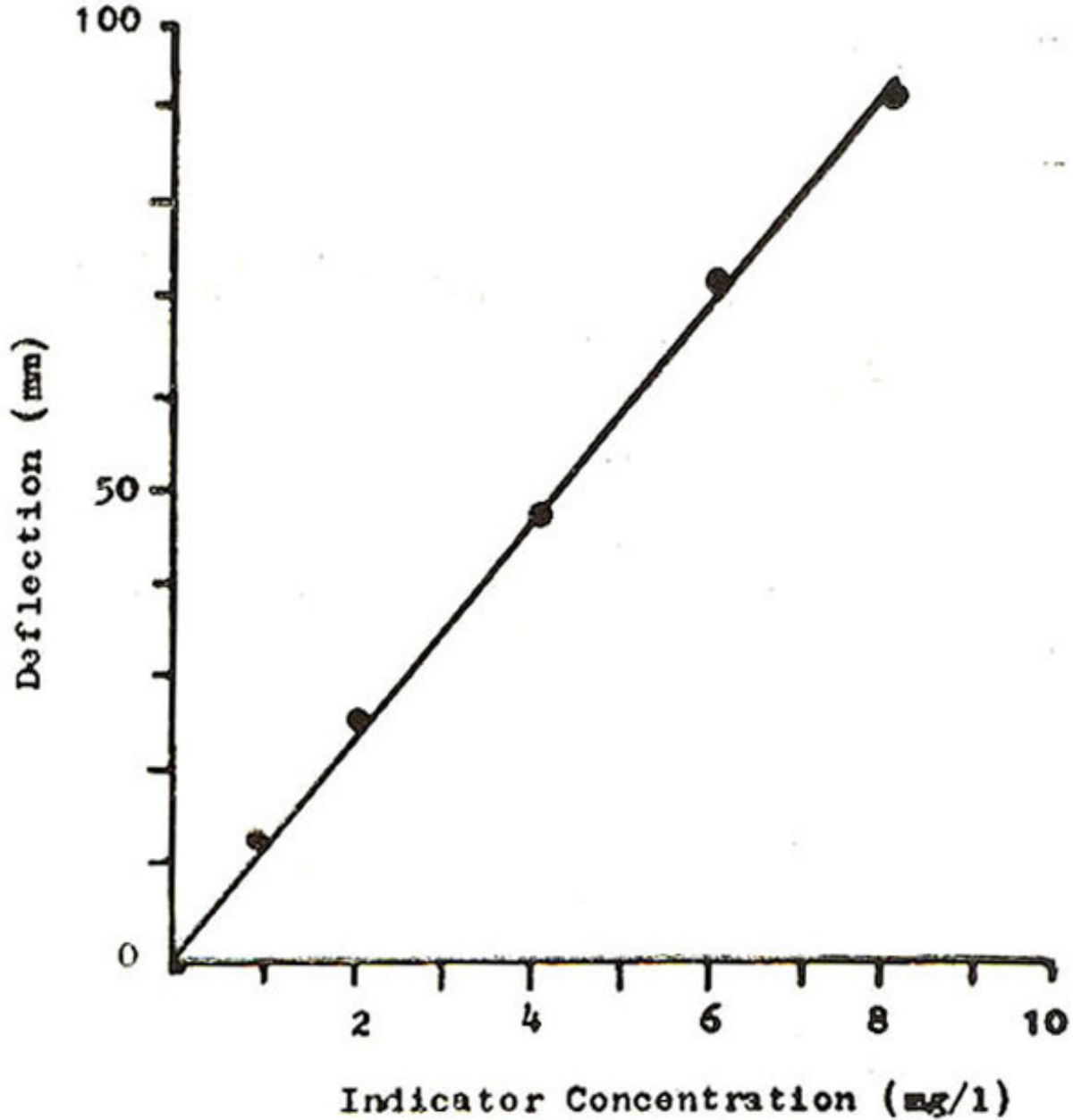
*Fig. 2.* Measured Concentration (mm/mg/L) of Indicator plotted against Time on Logarithmic axis. The solid line of Figure-2 is transferred to Figure-1 (dotted line).

Then the area under the curve (complete) planimeted and expressed in mm<sup>2</sup>.

(Indicator concentrations (mg/l)

The calibration factor  $k = \frac{\text{Area}}{\text{deflection}}$  correspondingly (mm)

was obtained by using calibration curve (Fig. 3)



*Fig. 3.* Calibration Curve obtained by Sampling of known Dilutions of the Indicator through Densitometer and Recording the Deflection.

obtained by sampling the known quantity of dye through densitometer and measuring the deflection in mm. The base of the curve is also measured in mm. Now by the following formula CO. can be calculated.

The area under the normal indicator dilution curve may be determined in several ways. One method is to utilize the sum of concentration time values (mm Sec) are read at one second intervals from the complete curve down to 1% of peak concentration. For this method the formula will be Where  $C_1 =$  the

sums of the concentration time value (mm sec) read at one second intervals. The other method is Dow's method (Dow, 1955) which calculates the whole curve area from the peak concentration (PC) Peak concentration time (PCT) appearance time (AT) and two constant namely 3 and 0.9. According to this method the formula will be (Fig. 1):-

**Choice of Indicator:-** The best indicator for general use in experimental studies is the Indocyanine Green (cardiogreen), being non toxic even in larger doses and without adverse effects on the cardiovascular system (Kelman, 1971). It remains in circulation during its passage through the pulmonary capillaries. This dye is, however, expensive and unstable in aqueous solution.

Cold saline or Coolth is also a useful indicator. It is simple, inexpensive and nontoxic. The accuracy of the technique using Coolth depends on no loss of Coolth occurring between the injection and measuring points.

A simple method has been devised to measure the cardiac output by using thermistor probe and cold saline. The equation used for calculating the cardiac output is as follows (Moore et al., 1929):-  $f$  can be calculated at the end of the experiment by putting the thermistor probe (carotid probe only) into a beaker of saline at known temperature and deflection of the pen of the recorder was noted. From these values a graph can be plotted mm/oc from which the slope can be determined for use.

Radioactive microsphere are also in use for the measurement of CO. McDevitt and Nies (1976) showed in rat that simultaneous estimate-can be made by injecting" the carbonized microspheres labelled with  $^{85}\text{Sr}$  (15u diameter) in left ventricle over 20S and arterial blood was withdrawn from the femoral artery at 0.8 ml/min for 90 sec. This reference sample was used to calculate the CO by the formula

$\text{C.O} = \frac{\text{Counts injected} \times \text{reference saw pie withdrawal rate}}{\text{reference sample rate}}$

The radioactivity of the microspheres was determined by gamma scintillation counting before and after injection. The difference showed the amount of radioactivity injected.

**3. Pulse contour method:-** Erlanger and Flooker (1904) recognised that the product of the pulse pressure and the heart rate indicated C.O., but with some reservations. There is a clear relationship between left ventricular stroke volume (SV) and the variation of aortic blood pressure during the cardiac cycle. When there is an increase in pulse pressure there should be an increase in SV. By recording the pulse pressure, it is theoretically possible to estimate continuously the SV and so of C.O. (Kelman, 1971).

This method gives beat-by-beat estimate of cardiac output but proved unsatisfactory for precise definition of the mathematical relationship between SV and pulse pressure (Rushmer, 1970).

**4. Ballisto-Cardiography:-** When the ven tricular contents are discharged into the arterial tree during systole, the remainder of the body experiences force in the opposite direction. The forces arising from the heart's action may be recorded by placing the oodv on a horizontally suspended platform equipped with means of measuring its movements. This record is known as ballistocardiograms (BCG). Many workers attempted to relate the magnitude of the BCG to SV. Most have concluded that this relationship is qualitative rather than quantitative.

**5. Catheter Flowmeters:-** There are various kind of flowmeters available hut their use is restricted to the animal research. These types are 1) Electro magnetic flowmeters, 2) Thin Film.

Electromagnetic flowmeters consist of a cuft placed around the exposed artery in art experimental animal. A modification of this probe can easily be used in intact subjects, which has been developed in a way that such a flowmeter has been turned inside out so that blood flows over the surface of electromagnet and this flow causes an induced potential difference (PD) proportional to the flow velocity in the vicinity of the surface of the probe and this P1) can be detected with electrodes and, with the knowledge of the vessels cross sectional area, it is possible to calculate the total blood flow/mm.

Thin film catheter consists of a thin metal film, is deposited on the catheter and this catheter can be passed through the artery percutaneously. An electric current passed through the film raises the temperature, and blood flow over this surface removes the heat by convection. The temperature of the film (its electrical resistance) thus gives a measure of blood flow.



In conclusion, the indicator dilution method seems to be better than others described above. In experimental studies flowmeters method may not be physiological as such that the opening of the chest of the animals is involved for the placement of the cuff round the aorta. Moreover it cannot be used in routine experimental studies due to lengthy surgical intervention. Ballistocardiography has not been reported in animal studies and it requires elaborate apparatus, even in clinical situation this method is more qualitative than quantitative (Kelman, 1971). Another drawback in this method is that the results may be seriously distorted by such factors as coupling between the body and the table, the elasticity of the skin acts as a spring interposed between the moving body, and the table top.

The Fick method although reliable is complicated and time consuming. One aspect in particular is hazardous in clinical situation, the cardiac catheterization. In experimental studies this method will not be able to give results continuously with the changes in CO as the measurements will be intermittent. The pulse contour method can give beat-to-beat measurement of C.O but to define the precise mathematical relationship between stroke volume and pulse pressure have proved unsatisfactory. When three methods have been compared, viz; pulse contour method, thermodilution coil saline was used and flowmeter method, the results showed that determination by mathematical index (Pulse contour method) resulted in lower values for C.O., while thermodilution technique showed good correlation to values obtained by electromagnetic flowmetry. The thermodilution method has the advantage, however, of being less invasive than the electromagnetic flow method and provides absolute flow values unlike the index. The main disadvantage of thermodilution is that continual readings can not be made.

## II. First Derivative of the Ventricular Pressure.

The first time derivative of the ventricular pressure is "the rate of change of pressure with respect to time" and usually expressed as  $dP/dt$ . Maximum value attained during early systole is designated as peak  $dP/dt$  (Yang et al., 1972 b). The maximal rate of left ventricular pressure rise (Max  $dP/dt$  and value derived from it have been used to evaluate the inotropic state of the heart in clinical Gleason and Braunwald, 1962; Mason, 1969) and in experimental situations (Reeves et al., 1960; Schaper et al., 1965).

The peak  $dP/dt$  has been used in the assessment of myocardial function, as it increases with increased contractility by digitalis action and the depressed myocardial contractility depresses the peak  $dP/dt$ . However, peak  $dP/dt$  also affected by the factors which are not related to the inotropic changes. Principal among these factors which alter peak  $dP/dt$  when contractility is stable are the loading conditions under which the heart operates. These loading conditions are: (Braunwald et al., 1976a):-  
**Preload:-** In the intact heart ventricular end-diastolic wall stress or tension is called- pre-load and determines the resting length of the muscle fibre. This preload on ventricular muscle can be altered (increased or decreased) by changing the end-diastolic pressure EDP and volume. It has been shown that increase in LVEDP also increased the peak  $dP/dt$  (Wallace et al., 1963; Robie and Newman, 1975).  
**Afterload:** It may be defined as the tension, force or stress in the ventricular wall during ventricular ejection (Braunwald et al., 1976b). Arterial diastolic pressure is a determinant of ventricular afterload (Mason, 1969). Elevation of arterial diastolic pressure influence the rate of rise of ventricular pressure during systole (Wallace et al., 1963; Wildenthal et al., 1969).

The other factor which effects  $dP/dt$  is heart rate. Any increase in heart rate causes an increase in the rate of rise of the ventricular pressure. Inherently related to an elevation of heart rate is an improvement in the fundamental contractile properties of the heart rate (Wallace et al., 1963). A direct linear correlation has been determined between peak  $dP/dt$  and heart rate in a variably paced canine atrial preparation (Wallace et al., 1963).

The development of indices to estimate contractility ( $dP/dt$ ).

The various indices used to estimate contractility by indirect means in either anaesthetized or conscious animals based on the appreciation of correction factors, which mainly concern the effect of loading condition (such as preload and afterload) of the heart. The following indices have been

developed to separate the effect of preload conditions on  $dP/dt$  from the effect of changes in contractility on  $dP/dt$  when afterload remains constant.

**Time to peak  $dP/dt$ :**- The time interval from the onset of ventricular contraction to the  $dP/dt$  max. denotes time to peak  $dP/dt$  ( $t$ -peak  $dP/dt$ ) (Mason, 1969). It has been shown in intact canine preparations that, when  $t$ -peak  $dP/dt$  is shortened the peak  $dP/dt$  increases and an augmentation of myocardial contractility is seen to occur (Mason et al., 1965). The combination of  $t$ -peak  $dP/dt$  allows a more precise estimation of directional changes in contractility than peak  $dP/dt$  used SC paratci V. Isometric tension (Pressure) and end-diastolic pressure:- Another index of myocardial contractility has been based on the way in which alterations of end-diastolic fibre length of ventricular muscle affect the in-otropic state (Mason, 1969). It has been demonstrated that a constant fraction of integrated systolic isometric tension (IIT) and the rate of development of isometric tension in isolated cat papillary muscle and the pressure in the isovolumic canine heart varies directly with changes in end-diastolic length of the fibre (Siegal and Sonnenblick, 1963).

When the measurements were made in the intact heart the ratio of peak  $dP/dt$ /IIT of the isolated papillary muscle is replaced by the ratio of peak  $dP/dt$ /IIP for the assessment of contractility free of changes in end-diastolic volume. The ratio of the  $dP/dt$ /IIT or  $dP/dt$ /IIP is not affected by the magnitude of the preload (or fibre length) at a given stimulation rate but only myocardial contractility (Seigal and Sonnenblick, 1963).

**Peak  $dP/dt$ /LVEDP (left ventricular end-diastolic pressure):**- This index has been advocated for measuring the contractility by Reeves et al. (1960). They showed a significant correlation between maximum rate of pressure rise with ventricular end-diastolic pressure ( $r = .468$ ). This index is influenced by changes of arterial diastolic pressure (afterload).

**Peak  $dP/dt$ /LVEDV (Left ventricular end-diastolic volume):**- This index has shown in dogs a fairly good correlation with myocardial contractility. But much overlapping has been reported with control state and with increased afterload (Braunwaki et al., 1969). In hypertrophy condition in which increased muscular mass tends to raise peak  $dP/dt$  this index could falsely suggest just the opposite (Yang et al., 1972b).

**$dP/dt$ /MIT:**- Frank and Levinson (1964) suggested that the ratio of peak  $dP/dt$  to maximal isovolumic tension (MIT) is useful as an index of contractility. MIT can be calculated from the determination of end-diastolic volume and peak isovolumic pressure. This MIT can be substituted with MIP and can be defined as the highest isovolumic left ventricular pressure in mmHg. This index has been proposed as a result of the observations that the index  $dP/dt$ /IP showed a significant correlation with fibre length (Yang et al., 1972b).

**Correction Factor for afterloads:**- The parameter derived from the peak  $dP/dt$  which corrects for afterload is denoted as  $cIP/dt$ /CPIP. CPIP is the maximal developed isovolumic pressure in mmHg which is common to both control and the altered state  $dP/dt$  is the rate of development of pressure in mmHg/ sec at the instant CPIP obtains for each state.

The above concept (that the relation between  $dP/dt$  and developed pressure throughout the course of isovolumic contraction) has been formulated, in an attempt to provide an accurate measure of ventricular contractility independent of afterload (changes of arterial pressure). For these studies and intact canine left ventricular preparation was prepared with a right heart by pass in which ventricular end-diastolic and aortic pressures, heart rate and the contractile state could be controlled independently (Mason et al., 1967). When the aortic diastolic pressure (afterload) was altered even a very wide range and other parameters were kept constant, it was observed that the relationship of  $dP/dt$  to developed isovolumic pressure was not influenced by the pressure at which the aortic valve opened.

In conclusion peak  $dP/dt$  (maximum rate of rise of the ventricular pressure) is dependent on the loading conditions (preload and afterload) of the heart, heart rate and contractile state of the ventricle. When the loading conditions are stable peak  $dP/dt$  provides a sensitive means for the evaluation of changes in contractility. The elevation of ventricular end-diastolic (preload) or aortic diastolic pressure

(afterload) result in elevations of peak  $dP/dt$ . It has been shown in isolated papillary muscle and intact canine ventricles that, when preload is stable and afterload varies the effect of variation or aortic diastolic pressure on  $dP/dt$  can be neutralized by comparing  $dP/dt$  at common isovolumic pressures. In this way a simple and useful method for the assessment of myocardial contractility during alterations of afterload has been provided.

The methods for measuring the cardiac performance which have been discussed are not free from criticism, especially the incorporation of the findings in isolated cardiac muscle preparation (Papillary muscle to the intact heart). Brutsaort and Paulus (1977) pointed out that pragmatic usefulness being only the justification for applying isolated muscle concept to the intact ventricle is no longer a sufficient argument.

The ventricle function is as a combined muscle-pump system and not as a papillary muscle and even less a simple tension muscle. The nature of loading forces which occur during muscle shortening in the ventricular wall in intact heart are quite different from those encountered in isolated muscle since the ventricle is not called on to sustain a weight but to eject a viscous fluid into a viscoelastic vascular system (Abbott and Gordon, 1975).

Moreover difficulties have been reported of attempts to use the method of extrapolating the plot of LV  $dP/dt$  against  $P$  to Zero  $P$  to obtain  $V_{max}$  (Van Den Bos et al., 1973). Suggestions have been put forward to make progress in the field of measurement of ventricular function by conducting experiments that should be designed to distinguish between the relative contributions of muscular mechanisms and those of the ventricular configurational mechanisms underlying Starling's law of the heart (Brutsaort and Paulus, 1977). However so far the index of  $V_{max}$  has been favoured both in animals (Nejad et al., 1971) and in the clinic (Mason et al., 1970) as a suitable and accurate method determining the rate of rise of pressure in ventricles.

## References

1. Abbott, B.C. and Gordon, D.G. (1975) A commentary on muscle mechanics. *Circ. Res.*, 36:1.
2. Astrand, P.O., Cuddy, T.E., Saltin, B. and Stenberg, J. (1964) Cardiac output during submaximal and maximal work. *J. Appl. Physiol.*, 19:268.
3. Bousvaros, G.A., Done, and Hopps, J.A. (1962) An electrical hazard of selective angiocardiology. *Canad. Med. Ass. J.*, 87 :286.
4. Braunwald, E., Ross, J. Jr., Gault, J.H., Mason, D.T., Mills, C., Gabe, I.T. and Epstein, S.E. (1969) Assessment of cardiac function. *Ann. Intern. Med.*, 70:369.
5. Braunwald, E., Ross, J. Jr. and Sonnenblick, E.H. Mechanics of contraction, in mechanisms of contracting of the normal and failing heart. Little Brown, 1976, pp. 39-71.
6. Braunwald, E., Ross, J. Jr. and Sonnenblick, E.H. Mechanism governing contractions of the whole heart, mechanisms of contracting of the normal and failing heart. Little Brown, 1976, pp. 92-129.
7. Brutsaort, D.L. and Paulus, W.J. (1977) Loading and performance of the heart as a muscle and pump. *Cardiovasc. Res.*, II:1.
8. Dow, P. (1955) Dimensional relationships in dye-dilution curves from humans and dogs, with an empirical formula for certain troublesome curves. *J. Appl. Physiol.*, 7:399.
9. Erlanger, J. and Hooker, D.R. (1904) An experimental study of blood pressure and of pulse pressure in man. *Johns Hopkins Hosp. Rep.*, 12:145. (Quoted from Rushmer, R.F. (1970)).
10. Fick, A. (1870) Über die messung des Blutquantums der Herzventrikel. *S.B. Phys-Med. Ges. Wurzburg* 16 (Quoted from Yang et al., 1972).
11. Frank, M.J. and Levinson, G.E. (1964) Measurement of myocardial contractility in man. *Clin. Res.*, 12:182.
12. Gleason, W.L. and Braunwald, E. (1962) Studies on the first derivative of the ventricular pressure

pulse in man. *J. Clin. Invest.*, 41:80.

13. Hamilton, W.F. and Remington, J.W. (1948) Comparison of time concentration curves in arterial blood of diffusible and non-diffusible substances when injected at constant rate and when injected instantaneously. *Am. J. Physiol.*, 148 :3 5.
14. Kelman, G.R. Cardiovascular measurements, in applied cardiovascular physiology. London, Butterworth, 1971, pp. 210-242.
15. Kinsman, J.M., Moore, J.W. and Hamilton, W.F. (1929) Studies on the circulation; injection method: physical and mathematical consideration. *Am. J. Physiol.*, 89: 321-330.
16. Mason, D.T. (1969) Usefulness and limitation of the rate of rise of intraventricular pressure (dp/dt) in the evaluation of myocardial contractility in man. *Am. J. Cardiol.*, 23 :516.
17. Mason, D.T., Sonnenblick, K.U., Ross, J. Jr., Covell, J.W. and Braunwald, K (1965) Time to peak dp/dt: A useful measurement for evaluating the contractile state of the human heart. *Circulation*, 32 (Suppl II): 145.
18. Mason, D.T., Sonnenblick, E.H., Covell, J.W., Ross, J. Jr. and Braunwald, E. (1967) Assessment of myocardial contractility in man relationship between the rate of pressure rise and developed pressure throughout isometric left ventricular contraction. *Circulation*, 36 (Suppl II) :183.
19. Mason, D.T., Spann, J.F. Jr. and Zelis, R. (1970) Quantification of the contractile state of the intact human heart. Maximal velocity of contractile element shortening determined by the instantaneous relation between the rate of pressure rise and pressure in left ventricle during isovolumic systole. *Am J. Cardiol.*, 26:248.
20. McDevitt, D.G. and Nies, A.S. (1976) Simultaneous measurement of cardiac output and its distribution with microspheres in rat. *Cardiovasc. Res.*, 10:494.
21. Moore, J.W., Kinsman, J.M., Hamilton, W.F. and Spurling, R.G. (1929) The circulation. II. Cardiac output demonstrations; comparison of the injection method with the direct Fick procedure. *Am. Physiol.*, 89:331.
22. Nejad, N.S., Klein, M.D., Mirsky, I. and Lown, B. (1971) Assessment of myocardial contractility from ventricular pressure recordings. *Cardiovasc. Res.*, 5:15.
23. Reeves, T.J., Hefner, L.L., Jones, W.B., Coghlan, U., Prieto, G. and Carroll, J. (1960) The haemodynamic determinants of the rate of change in pressure in the left ventricle during isometric contraction. *Am. Heart J.*, 60:745.
24. Robie, N.W. and Newman, W.H. (1975) The influence of preload measured as diastolic mural force, on myocardial contractility indices. *Proc. Soc. Exp. Biol. Med.*, 148:69.
25. Rushmer, R.F. Cardiovascular dynamics. 3rd ed. Philadelphia, Saunders, 1970.
26. Schaper, W.K.A., Lewis, P. and Jageneau, A.H.M. (1965) The determinants of the rate of change of the left ventricular pressure (dp/dt). *Arch. Kreislaufforsch.*, 46:27.
27. Siegel, J.H. and Sonnenblick, E.H. (1963-) Isometric time-tension relationships as an index of myocardial contractility. *Circ. Res.*, 12:597.
28. Stewart, G.N. (1897) Researches on the circulation time and on the influences which effect it. IV. The output of the heart. *J. Physiol.*, 22:159. (Quoted from Yang et al., 1972),
29. Stewart, U.N. (1921) The output of the heart in dogs. *Am. J. Physiol.*, 57:27. (Quoted from Yang et al., 1972).
30. Stow, R.W. (1954) Systematic errors in flow determinations by the Fick method. *Minnesota Med.*, 37:30.
31. Van Den Bos, G.C., Elzinga, G., Westerhoff, N. and Noble, M.I.M. (1973) Problems in the use of indices of myocardial contractility. *Cardiovasc. Res.*, 7:834.
32. Wallace, A.G., Skinner, N.S. Jr. and Mitchell, J.H. (1963) Haemodynamic determinants of the maximal rate of rise of left ventricular pressure. *Am. J. Physiol.*, 205:30.
32. Wildenthal, K., Mierzwia, D.S. and Mitchell, J.H. (1969) Effect of sudden changes in aortic pressure on left ventricular dp/dt. *Am. J. Physiol.*, 216:185.

34. Yang, S.S., Bentivoglio, L.G., Maranhao, -V. and Goldberg, H. Cardiac output, in cardiac catheterization data to haemodynamic parameters. Philadelphia, Davis, 1972, pp. 21-36.
35. Yang, S.S., Bentivoglio, L.G., Maranhao, V. and Goldberg, H. Assessment of ventricular function, in cardiac catheterization data to haemodynamic parameters. Philadelphia, Davis, 1972, pp. 157-.-210.
36. Zierler, K.L. Circulation times and the theory of indicator-dilution methods for determining blood flow and volume, in hand book of physiology. Sec. 2, vol. 1. washington, American Physiological Society, 1962, p. 585.